

Effect of Surfactants' Tail Number on the PVDF/GO/TiO₂-Based Nanofiltration Membrane for Dye Rejection and Antifouling Performance Improvement

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RESEARCH PAPER

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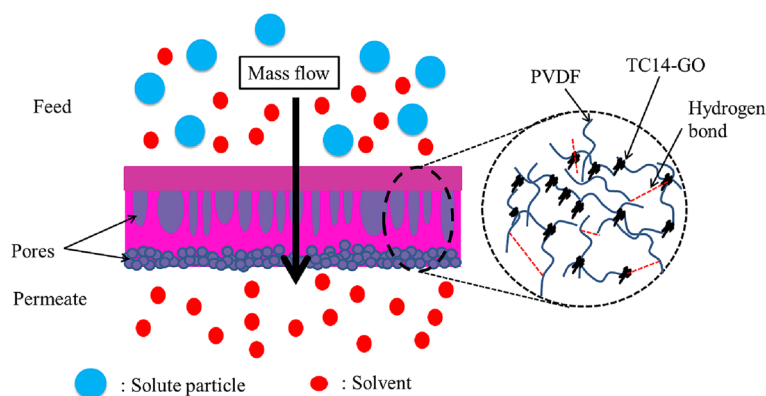
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Abstract

In this work, the novel utilisation of customised double- and triple-tail sodium *bis*(3,5,5-trimethyl-1-hexyl) sulphosuccinate (AOT4) and sodium 1,4-*bis*(neopentyloxy)-3-(neopentyloxycarbonyl)-1,4-dioxobutane-2-silphonate (TC14) surfactants to assist the direct graphene oxide (GO) synthesis via electrochemical exfoliation utilising dimethylacetamide (DMAc) as a solvent were investigated. The synthesised DMAc-based GO and titanium dioxide (TiO₂) nanoparticles were then used to fabricate polyvinylidene fluoride (PVDF)-based nanofiltration (NF) membranes by the non-solvent-induced phase separation method. The incorporation of GO and TiO₂ as hydrophilic nanoparticles were to enhance membrane hydrophilicity. The utilisation of higher surfactants' tail number obviously alters the fabricated membrane's morphology which further affects its performance for dye rejection and antifouling ability. Higher surfactants' tail number resulted in higher oxidation process which then provided more interaction between the GO and PVDF. Based on the dead-end cell measurement, PVDF/TC14-GO/TiO₂ presented a slightly higher dye rejection efficiency of 92.61% as compared to PVDF/AOT4-GO/TiO₂ membrane (92.39%). However, PVDF/TC14-GO/TiO₂ possessed three times higher water permeability (48.968 L/m² h MPa) than PVDF/AOT4-GO/TiO₂ (16.533 L/m² h MPa) and also higher hydrophilicity as presented by lower contact angle (65.4 ± 0.17°). This confirmed that higher surfactants' tail number improved the fabricated membrane's performance. Both fabricated membranes also exhibited high flux recovery ratio (FRR) (> 100%) which indicated better antifouling properties.

Graphic abstract



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Article Highlights

- High dye rejection by using simpler electrochemical exfoliation utilising surfactant for GO synthesis.
- Improved water permeability by utilising triple-tail-based GO.
- Enhanced hydrophilicity by utilising triple-tail-based GO.
- Higher membrane porosity by utilising triple-tail-based GO.
- High antifouling performance by different surfactants' tail number.

Keywords Dye rejection · Electrochemical exfoliation · Graphene oxide · Hyper-branched surfactant · Nanofiltration · Titanium dioxide

Introduction

The rapid growth of various industries such as paints, textile, printing inks, paper, and plastics causes both high polluted water and high demand for clean water, simultaneously. These industries, especially textile and dyeing industries utilised a large amount of synthetic dyes to colour their product which resulted in large amount of polluted wastewater and released to the environment. Dyes presence can affect water quality since they are toxic and non-biodegradable (Liu et al. 2019; Tran et al. 2019; Yao et al. 2015). Therefore, the removal of this kind of pollutant is crucially needed. Numerous approaches have been attempted to find an effective method to treat polluted water to protect human health and the environment (Santhosh et al. 2016). Among various dye removal methods, membrane separation is one of the versatile and effective technologies to remove polluted water, such as dye contamination (García et al. 2020; Liu et al. 2017). This was due to its several advantages, such as no phase changes, simple in operation, and relatively low energy consumption (Kang and Cao 2014). Over the past few decades, it becomes popular and plays an important role in major industries for water purification, metal recovery and protein separation (Escobar and Van Der Bruggen 2015).

Membrane separation technology has become promising in many type of filtration such as microfiltration, ultrafiltration (UF), nanofiltration (NF), and reverse osmosis (RO). All of these types of filtration are classified based on their membrane properties and separation principle. Recently, the NF membrane has widely applied for water treatment due to its small pore size (1–5 nm) compared to UF, low operating pressure (4–20 MPa) and high water permeability than RO and its capability to retain high valence ions and low molecular weight (Park et al. 2012; Shon et al. 2013). The polymeric membrane can be fabricated by different technique such as sintering, stretching, track-etching and phase inversion (Liao et al. 2018). Among them, the phase inversion method is commonly used due to its several advantages, such as applicable for various polymers, simple in preparation and easy optimisation of membrane thickness and pore size (Ladewig & Al-Shaeli, 2017; Sangermano et al. 2015).

Synthetic polymer membrane namely polyvinylidene fluoride (PVDF), a semicrystalline polymer with repeating units of $-\text{CH}_2-\text{CF}_2-$, has been extensively used in water treatment processes due to its outstanding physical and chemical properties (Aid et al. 2019; Anvari et al. 2017; Contreras et al. 2018; Kang and Cao 2014; Sangermano et al. 2015). However, the hydrophobic nature of the PVDF membrane causes some critical problems which limit its application due to the membrane fouling during the separation process (Li et al. 2015; Wu et al. 2018). The membrane fouling causes the decline in water flux permeability, shortening membrane lifetime and altering membrane selectivity thus decreased the membrane performance (Teng et al. 2020; Wu et al. 2020; Zhang et al. 2016). Therefore, several approaches have been developed to increase the hydrophilicity properties of PVDF membrane such as physical and chemical modification with hydrophilic organic and inorganic materials (Kang and Cao 2014; Xia and Ni 2014). Among these approaches, a physical modification of blending with organic or inorganic materials has been widely used due to its advantage of facile preparation method through phase inversion. Recently, organic materials-blended PVDF (PMMA, PVAC, PA6) (Freire et al. 2012; Vo and Giannelis 2007), metal oxide particles [aluminium oxide (Al_2O_3), titanium dioxide (TiO_2) and zinc oxide (ZnO)] (Li et al. 2015; Liu et al. 2018), carbon nanotubes (CNTs) (Sivakumaran et al. 2016; Zheng et al. 2009) and graphene oxide (GO) (Wu et al. 2018) have been utilised to enhance the PVDF membrane properties by increasing antifouling effect, permeability and membrane selectivity.

In particular, a potential candidate to effectively reinforce PVDF polymeric materials is TiO_2 due to its excellent properties such as hydrophilicity, chemical stability, low toxicity and commercial availability. TiO_2 is considered the best metal oxide to overcome the fouling issues by increasing the membrane hydrophilicity (Liu et al. 2018; Wu et al. 2018). In addition, it also possesses a small particle size and a large surface area (Park et al. 2018). Several reports have demonstrated that the utilisation of TiO_2 could improve the fouling resistance by increasing the membrane hydrophilicity. Wang et al. (2017) showed that introduction of TiO_2 into the GO-based membrane presents low relative flux reduction (24%)

as compared to pristine GO-based membrane (74%). This low value in relative flux reduction indicates a great anti-fouling property (Wang et al. 2015). The result obtained by Zhang et al. (2017) showed an improvement in antifouling properties when the Ti and O element on the membrane increased as compared to the pristine membrane. This indicated that the hydrophilicity of the membrane was enhanced with the TiO_2 present (Zhang et al. 2017). Méricq et al. (2015) also showed the improvement of membrane structure, hydrophilicity properties and permeability when TiO_2 nanoparticles were used as an additive for membrane fabrication.

On the other side, GO was also utilised as an additive to fabricate a hydrophilic membrane. GO offers many advantages for water treatment due to its large surface area (calculated up to $2630 \text{ m}^2\text{g}^{-1}$) (Huang et al. 2012), good chemical stability and high mechanical strength (Young modulus $\sim 1 \text{ TPa}$) (Lee et al. 2008). As exfoliated GO contains a considerable number of oxygen-functional groups, such as carboxyl, carbonyl, epoxy, and hydroxyl groups, GO is highly hydrophilic (Miao et al. 2017; Zhang et al. 2013). GO can be synthesised by using a chemical approach, such as Hummers' method and electrochemical exfoliation. The common Hummers' method resulted a high quality of the synthesised GO. However, this method involved high hazardous chemical consumption, long-time production and complicated procedures (Zaaba et al. 2017). A low cost and simpler GO synthesis approach, which is an electrochemical exfoliation method assisted by surfactant then offers several advantages such as greener, simpler and low-cost production to synthesise GO (Nurhafizah et al. 2015; Parvez et al. 2013; Suriani et al. 2019). Many reports of GO-incorporated membranes for wastewater treatment systems have also successfully increased rejection for different heavy metals (Kochameshki et al. 2017) and dye pollutants (Safarpour et al. 2016; Yang et al. 2017; Zhu et al. 2017). Nonetheless, the agglomeration of GO is the major drawback in the development of GO/PVDF membrane, which can reduce its performance. To prevent GO from agglomeration, the utilisation of surfactant for better dispersion of GO in the polymer matrix is essentially needed.

The previous report showed that the highest CNTs dispersion was achieved by using the triple-tail sodium 1,4-bis(neopentyloxy)-3-(neopentyloxycarbonyl)-1,4-dioxobutane-2-silphonate (TC14) surfactant as compared to single- or double-tail surfactant (Mohamed et al. 2014). Suriani et al. (2016) showed that the utilisation of triple-tail TC14 surfactant has presented a smooth surface with low agglomeration of GO when the synthesised GO was inter-mixed with natural rubber latex. The triple-tail surfactant offers triple interaction during electrochemical exfoliation which resulted in higher dispersion of GO. This result was also in good agreement when the synthesised GO utilising triple-tail TC14 surfactant was used to fabricate thin film

and resulted in higher DSSCs efficiency as compared to the single-tail surfactant (Suriani et al. 2018a, b, c). These confirm that the surfactant's tail number essentially affects the quality of the synthesised GO.

The previous report has also proved that the direct GO synthesis utilising single-tail sodium dodecyl sulphate (SDS) surfactant and DMAc as solvent was successfully achieved and can be used to fabricate NF membrane which resulted in high dye rejection of 92.76% (Suriani et al. 2019). Therefore, it is believed that by using customised double-tail sodium bis(3,5,5-trimethyl-1-hexyl) sulphosuccinate (AOT4) and triple-tail TC14 surfactants, better dispersion and homogeneity of GO-based membrane sheet will be achieved and resulted to better performance for water treatment applications. To the best of our knowledge, the novelty of this study is the utilisation of customised double-tail AOT4 and triple-tail TC14 surfactant for the GO synthesis by electrochemical exfoliation method for dye rejection application. It is believed that the utilisation of both surfactants in the fabrication of the PVDF/GO-based hybrid membrane will increase the hydrophilicity, water flux, dye rejection and anti-fouling performance.

Materials and Methods

Materials

The customised double-tail AOT4 and triple-tail TC14 surfactants (see Table 1), graphite rods (99.99 %, 150 mm in length and 10 mm in diameter, GoodFellow GmbH, Germany) and DMAc were used for GO synthesis. PVDF (Kynar 760, grade in palette form) as a polymer material and titanium (IV) oxide ($\geq 99.5\%$, Sigma-Aldrich) as an additive were used to fabricate the NF membrane. Meanwhile, the MB dye (Sigma-Aldrich) was used for the dye rejection test.

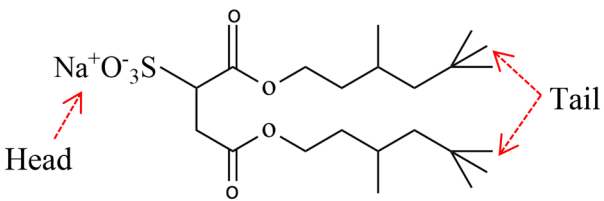
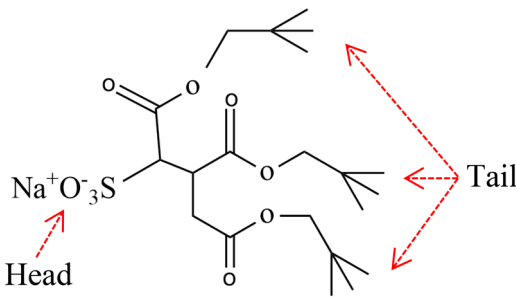
DMAc-Based GO Synthesis

GO was synthesised via electrochemical exfoliation as mentioned in the previous works (Suriani et al. 2018a, b, c) by utilising DMAc as an electrolyte. In brief, AOT4 and TC14 were dissolved in DMAc to form the 0.1 M of the electrolyte, respectively. Then, two graphite rods were partially immersed in the prepared electrolyte and connected to the DC power supply (7 V) for 24 h of GO synthesis time.

Preparation of NF Membranes

The NF membrane was prepared by the non-solvent induced phase separation (NIPS) method. 20 wt% of PVDF and 1 wt% of TiO_2 were dissolved to the 79 wt% of the synthesised DMAc_AOT4 and DMAc_TC14 solution, respectively and

Table 1 Surfactant's molecular structure used in this study

Surfactant	Surfactant molecular structure	Chemical name
AOT4		Sodium <i>bis</i> (3,5,5-trimethyl-1-hexyl) sulphasuccinate
TC14		Sodium 1,4- <i>bis</i> (neopentyloxy)-3-(neopentyloxycarbonyl)-1,4-dioxobutane-2-sulphonate

mechanically stirred at 70 °C for 48 h until a homogeneous solution was obtained. Then, the well-mixed casting solution was kept at room temperature overnight to remove the air bubbles. Next, the fully degassing membrane solution was cast using a casting knife on a clean glass plate with 200 μ m casting gap. Afterward, the casted membrane was directly immersed in deionised (DI) water overnight. The fabricated NF membrane was kept by soaking it in DI water until further characterisation.

Membrane Characterisation

The membrane surface and cross-section morphology were characterised by field emission scanning electron microscopy (Hitachi SU8020). Liquid nitrogen immersion was carried out prior to FESEM observation to crack the membrane samples and further coated with a thin sputtered gold layer. The elemental compositions of the samples were directly confirmed by an EDX instrument (Horiba EMAX). The structural properties of the fabricated NF membranes were studied using micro-Raman spectroscopy (Renishaw InVia microRaman System). Moreover, the hydrophilicity of the fabricated membranes was investigated using contact angle measurement by placing the dry membrane on a glass slide and conducting drop shape analysis (DSA100, Kruss GmbH, Germany). The membrane porosity was determined through the gravimetric method by using the following equation:

$$\varepsilon = \frac{(w_1 - w_2)/\rho_w}{[(w_1 - w_2)/\rho_w] + (w_2/\rho_p)} \times 100\%. \quad (1)$$

where ε is membrane porosity (%), w_1 and w_2 were the wet and dry membrane weights (g), respectively, ρ_w is the water density (0.998 g/cm³), and ρ_p is the PVDF density (1.78 g/cm³).

Water flux, dye rejection and antifouling measurement were evaluated using a dead-end stirred membrane evaluation cell system (Sterlitech HP4750) with a capacity of 300 mL and an effective area of 14.6 cm². All membrane samples were pressurised with DI water at 0.6 MPa for 30 min before measurement for the compression test. Then, water flux measurement was performed for 10 min measurement with 5 different pressure levels (0.1–0.5 MPa), respectively. The water flux was then estimated using the following equation:

$$J = \frac{V}{A\Delta t}. \quad (2)$$

where J is the permeated flux (L/m²h), V is the permeated water volume (m³), A is the membrane area (m²), and Δt is the operating time (h).

Next, the dye rejection test was performed by utilising 10 ppm concentration of MB solution. The absorbance of the treated dye solution was then measured using UV–Vis spectroscopy. The dye rejection efficiency was calculated using the following equation:

$$R(\%) = \left[1 - \frac{C_p}{C_o} \right] \times 100\%. \quad (3)$$

where R is the dye rejection efficiency (%), C_p is the permeate dye concentration (ppm), and C_o is the initial dye concentration (ppm). Subsequently, the antifouling measurement

was done by pressuring the post-treated membrane with DI water for 30 min before performing the water flux measurement at 0.2 MPa for 10 min. The flux recovery ratio (FRR) was calculated by the following formula:

$$\text{FRR} = \left[\frac{J_{w2}}{J_{w1}} \right] \times 100\%. \quad (4)$$

where FRR is the flux recovery ratio, J_{w1} and J_{w2} are water flux before and after measurement, respectively. Operations of some characterisation items can refer to the literatures (Li et al. 2020; Liu et al. 2020; Rao et al. 2020; Xu et al. 2021).

Results and Discussion

Morphological Properties of NF Membranes

FESEM analysis was carried out to investigate the surface and cross-section morphology of the fabricated NF membranes and the results are presented in Fig. 1. Based on Fig. 1a, AOT4-GO clearly spreads all over PVDF/AOT4-GO/TiO₂ sample (red arrows) and possess a smooth surface without any crack. This indicated good dispersion of GO in membrane matrix, good stability and durable surface of the fabricated NF membranes (Safarpour et al. 2016; Zinadini et al. 2014). By utilising higher magnification, it was also observed that PVDF/AOT4-GO/TiO₂ membrane's surface possessed pores with a diameter range from 27.8–59.5 nm (Fig. 1b). Based on its cross-section view, there are two layers which exhibited a typical asymmetric membrane structure formed for PVDF/AOT4-GO/TiO₂. As presented in Fig. 1c, PVDF/AOT4-GO/TiO₂ has a thin and dense skin layer which was supported by a macro-voids structure. The bottom sub-layer of this membrane is a sponge-like structure. Further EDX analysis also confirmed the presence of C, O, F, Na, S and Ti as the component of the fabricated NF membranes as depicted in Fig. 1d. PVDF/AOT4-GO/TiO₂ contains C and O atomic percentages of 36.95 and 0.97%, respectively. The existence of AOT4 in PVDF/AOT4-GO/TiO₂ sample also can be proven by the atomic percentage of Na and S (2.75 and 1.71%, respectively) in the fabricated membrane. Meanwhile, a low Au atomic percentage of around 1.15% was caused by the thin gold coating for FESEM analysis.

Next, Fig. 1e showed that the fabricated PVDF/TC14-GO/TiO₂ NF membrane also has a smooth surface without any agglomeration or crack. TC14-GO was also observed to be well-dispersed in the membrane matrix as shown by red arrows. According to Fig. 1f, the larger pore size of PVDF/TC14-GO/TiO₂ (27.8–91.3 nm) was clearly seen as compared to PVDF/AOT4-GO/TiO₂. This might be attributed to the effect of higher GO content in PVDF/TC14-GO/

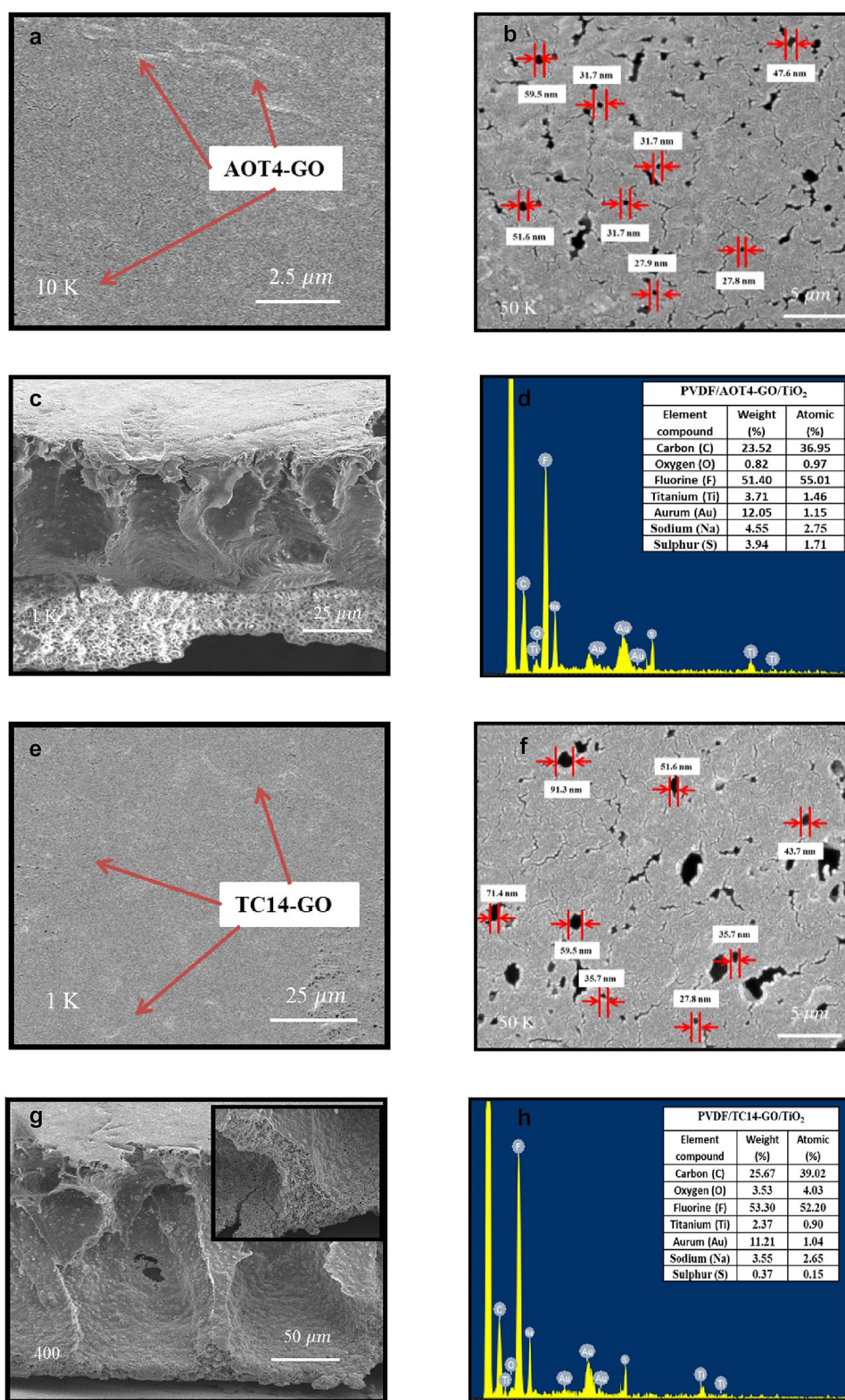
TiO₂ resulted from electrochemical exfoliation utilising higher surfactant's tail number. The PVDF/TC14-GO/TiO₂ NF membrane displayed a thin and dense skin layer with a well-developed of wider and longer macro-voids structure surrounded by sponge-like layer compared to PVDF/AOT4-GO/TiO₂ (Fig. 1g). In contrast with PVDF/AOT4-GO/TiO₂, the bottom sub-layer (sponge-like) of PVDF/TC14-GO/TiO₂ was almost unobservable (see insert picture) which might be caused by higher GO content in the sample (Zhu et al. 2017). In the previous study, it had been confirmed that the surfactant's tail-number influenced the quality of the synthesised GO (Suriani et al. 2018a). Higher surfactant's tail number in electrochemical exfoliation process was believed to also resulted in a higher amount of GO which noticeably influence the pores structure. The abundance hydrophilic group in GO (oxygen-functional groups) increased the membrane's hydrophilicity thus accelerated the water diffusion during the exchange of non-solvent and solvent and led to the formation of larger macro-voids structure (Méricq et al. 2015; Yang et al. 2017). EDX analysis further confirmed that PVDF/TC14-GO/TiO₂ presented a higher C and O atomic percentage (39.02 and 4.03%, respectively) as compared to PVDF/AOT4-GO/TiO₂ (Fig. 1h). The presence of Na (3.55%) and S (0.15%) further proved the existence of TC14 surfactant in the PVDF/TC14-GO/TiO₂ sample. A low Au atomic percentage of around 1.04% indicated the thin gold coating for FESEM analysis.

Functional Groups of NF Membranes

Raman spectroscopy is a useful technique to confirm the existence of GO in the fabricated membrane. Overall, micro-Raman spectra of both fabricated membranes showed a similar pattern as shown in Fig. 2. There are several peaks correspond to TiO₂ and GO in the range of 147.12–1579.80 cm⁻¹ which confirmed their existence as additives. However, PVDF peaks were unobservable for both membranes due to their low intensity as stated in the previous study (Suriani et al. 2019). TiO₂ peaks were observed at 147.12, 392.73, 510.35 and 635.19 cm⁻¹ and also 149.13, 396.69, 512.41, and 638.23 cm⁻¹ for PVDF/AOT4-GO/TiO₂ and PVDF/TC14-GO/TiO₂, respectively. These peaks were corresponding to the E_g , B_{1g} , A_{1g} and E_g modes of the anatase phase of TiO₂.

Moreover, micro-Raman spectra of D- and G-band as the characteristic of the carbon material were observed for both fabricated NF membranes. PVDF/AOT4-GO/TiO₂ and PVDF/TC14-GO/TiO₂ possessed the D- and G-band at 1330.55 and 1579.80 cm⁻¹ and also 1331.16 and 1579.37 cm⁻¹, respectively. The D-peak corresponded to the carbon lattice distortion, while G-peak confirmed the sp² hybridisation of the carbon atom (Ai et al. 2018). The shifted D- and G-band peak of PVDF/TC14-GO/TiO₂

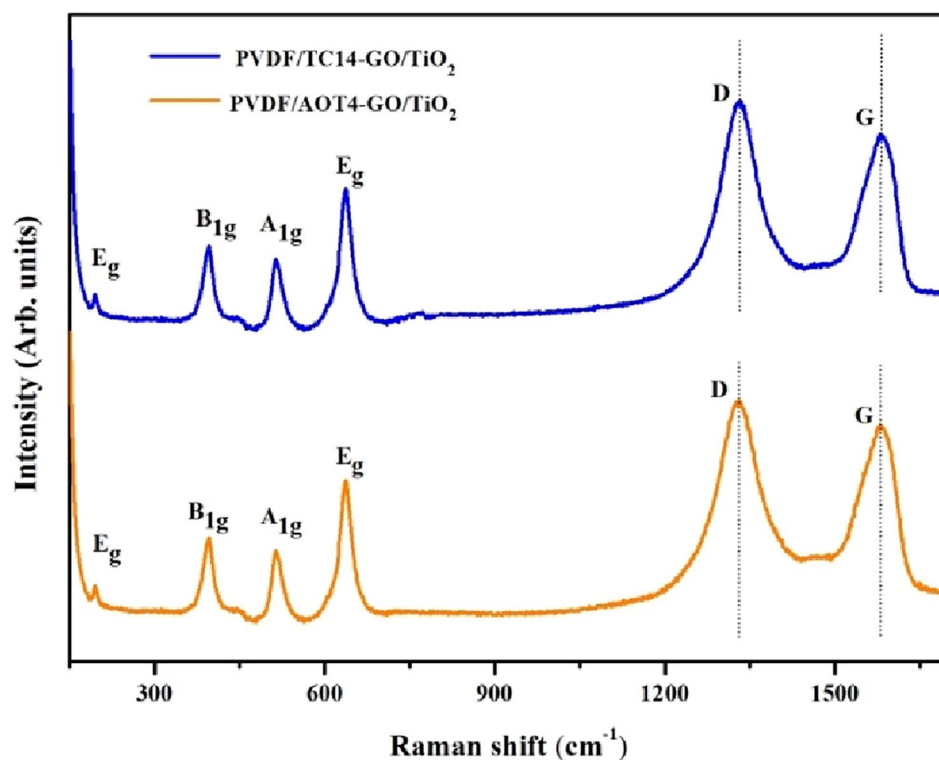
Fig. 1 FESEM images and EDX analysis of the fabricated NF membranes; (a–d) PVDF/AOT4-GO/TiO₂ and (e–h) PVDF/TC14-GO/TiO₂



compared to PVDF/AOT4-GO/TiO₂ was might be due to a higher oxidation process during electrochemical exfoliation resulted from higher surfactants' tail number. This was also confirmed by higher D-band peak intensity (I_D)

of PVDF/TC14-GO/TiO₂ compared to PVDF/AOT4-GO/TiO₂ which indicated a higher defect level (Khan et al. 2010). In addition, lower G-band peak intensity (I_G) of

Fig. 2 Micro-Raman spectra of the fabricated PVDF/AOT4-GO/TiO₂ and PVDF/TC14-GO/TiO₂ NF membrane



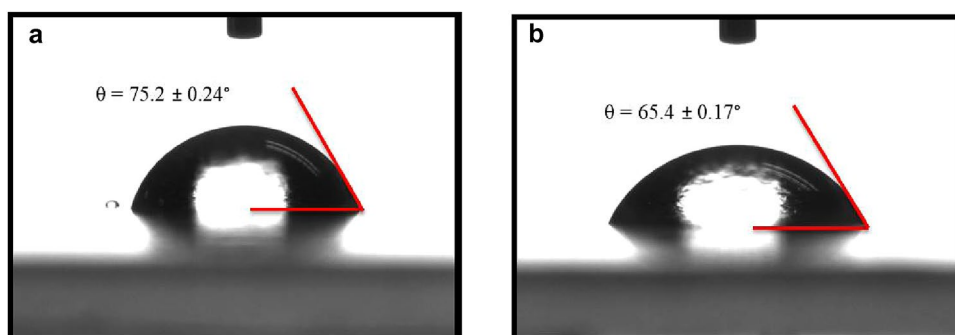
PVDF/TC14-GO/TiO₂ indicated a decreased number of exfoliated GO layer (Díez-Pascual et al. 2018).

I_D/I_G ratio can be used to investigate the defect level of the sample. Based on the calculation, PVDF/TC14-GO/TiO₂ presented a higher defect level of the synthesised GO which indicated by a higher I_D/I_G ratio (1.13) compared to PVDF/AOT4-GO/TiO₂ (1.06) (Francolini et al. 2019; Kaniyoor and Ramaprabhu 2012; Khan et al. 2010). In addition, it also showed higher oxygen-functional groups of PVDF/TC14-GO/TiO₂ resulted from electrochemical exfoliation than PVDF/AOT4-GO/TiO₂ (Francolini et al. 2019; Luo et al. 2018; Yu et al. 2015). This result further confirmed that the utilisation of triple-tail TC14 surfactant leads to higher interaction during GO synthesis thus resulted in better GO dispersion.

Hydrophilicity, Contact Angle and Porosity Properties of NF Membrane

Contact angle measurement was then used to investigate the membrane's surface hydrophilicity. From literature, pure PVDF have the highest contact angle (77.1°–104.3°) as compared to the hybrid membrane (Nikooe and Saljoughi 2017; Nor et al. 2016; Zhang et al. 2012; Zheng et al. 2016). It is well established that utilising the additive has an influence on the contact angle measurement. In comparison with pure PVDF in the previous study, both of the membranes presented smaller contact angle. However, as depicted in Fig. 3, PVDF/AOT4-GO/TiO₂ presented a higher contact angle value of $75.2 \pm 0.24^\circ$ (Fig. 3a) as compared to PVDF/TC14-GO/TiO₂ [$65.4 \pm 0.17^\circ$ (Fig. 3b)]. This indicated that membrane's hydrophilicity improved as the amount of GO

Fig. 3 Contact angle measurement of the fabricated; (a) PVDF/AOT4-GO/TiO₂ and (b) PVDF/TC14-GO/TiO₂ NF membrane



content in the PVDF/TC14-GO/TiO₂ membrane increased. This was believed due to the utilisation of triple-tail TC14 which provides an extra chain for GO and PVDF polymer interconnection (Lai et al. 2019). In addition, the abundance number of oxygen-containing functional groups of GO resulted in higher water molecule diffusion rate through the membrane caused by the hydrogen bond (Ai et al. 2018). As a result, the membrane becomes more hydrophilic and own a lower contact angle.

Further porosity measurement revealed that PVDF/TC14-GO/TiO₂ presented higher porosity (83.31%) as compared to PVDF/AOT4-GO/TiO₂ (79.35%). This result was in good agreement with FESEM images of PVDF/TC14-GO/TiO₂ (Fig. 1f) which shows a bigger pore size than PVDF/AOT4-GO/TiO₂ (Fig. 1b). Triple-tail TC14 surfactant plays a crucial role during the GO synthesis as a higher exfoliated GO amount was obtained compared to the double-tail AOT4 surfactant. Higher GO amount in PVDF/TC14-GO/TiO₂ sample leads to higher porosity and bigger pore size which increased the mass transfer rate between the solvent and the non-solvent during phase inversion (Zhu et al. 2017; Zinadini et al.

2014). In addition, higher porosity of the PVDF/TC14-GO/TiO₂ was might be caused by lower casting solution viscosity during the phase inversion process which then resulted in instantaneous demixing process (Ai et al. 2018). The contact angle and porosity value of the fabricated membranes are summarised in Table 2.

Water Flux of Fabricated Membranes Based on Different Operating Pressures

Pure water flux was measured to study the permeability of the prepared membranes. As presented in Fig. 4, water flux increased significantly with the increment of the operating pressure. As shown in Table 3, PVDF/TC14-GO/TiO₂ water permeability was observed to be three times higher (48.968 L/m² h MPa) as compared to PVDF/AOT4-GO/TiO₂ (16.533 L/m² h MPa) which was believed affected by its higher hydrophilicity and porosity. In addition, it also confirmed that higher water permeability of the fabricated NF membrane was achieved as GO content

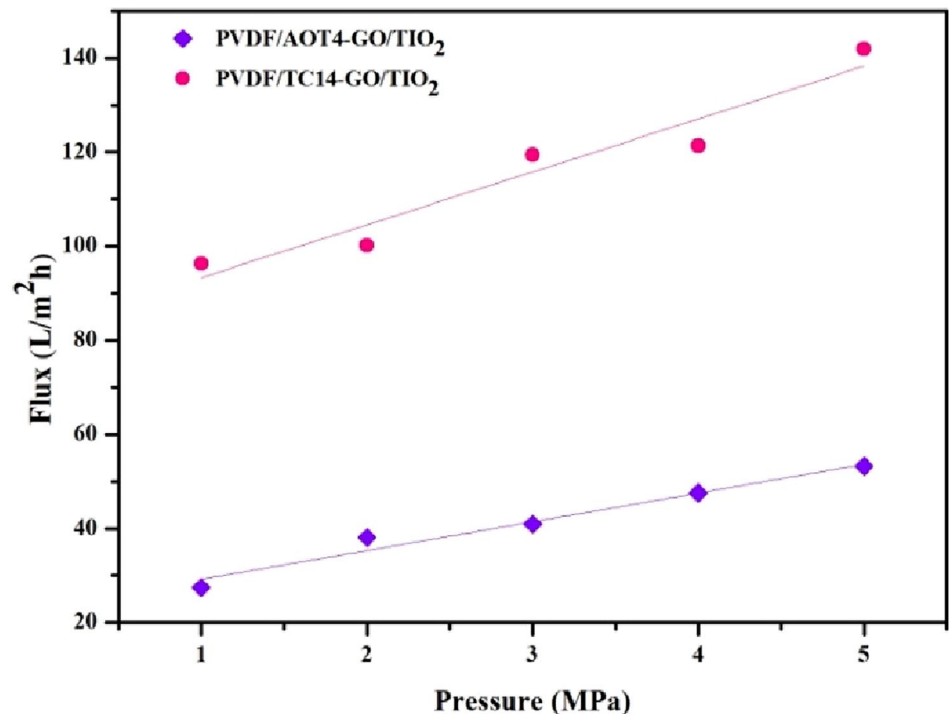
Table 2 Contact angle and porosity values of the fabricated NF membranes

Membrane	Contact angle (°)	Porosity (%)
PVDF/AOT4-GO/TiO ₂	75.2 ± 0.24	79.35
PVDF/TC14-GO/TiO ₂	65.4 ± 0.17	83.31

Table 3 Water permeability of the fabricated PVDF/AOT4-GO/TiO₂ and PVDF/TC14-GO/TiO₂ NF membranes

Membrane	Water permeability (L/m ² h MPa)
PVDF/AOT4-GO/TiO ₂	16.533
PVDF/TC14-GO/TiO ₂	48.968

Fig. 4 Water flux measurements of the fabricated NF membranes based on different driving pressure level



increased. The utilisation of triple-tail TC14 surfactant was believed resulted in higher exfoliated GO content as well as hydrophilic functional groups (PVDF/TC14-GO/TiO₂ sample) as compared to double-tail AOT4 surfactant (PVDF/TC14-GO/TiO₂ sample). This was also supported by the large macro-voids structure of PVDF/TC14-GO/TiO₂ (see FESEM images) which attracted and promoted the water molecules to pass through the membrane (Ai et al. 2018; Wang et al. 2018; Xia and Ni 2014). These results were also supported by membrane's pore sizes and pure water flux for both membranes.

Dye Rejection Performance of the Fabricated NF Membranes

Based on dead-end cell measurement, PVDF/TC14-GO/TiO₂ showed slightly higher dye rejection efficiency (*R*) value (92.61%) as compared to PVDF/AOT4-GO/TiO₂ membrane (92.39%) as shown in Fig. 5. However, PVDF/TC14-GO/TiO₂ possessed three times higher dye flux (91.106 L/m² h) as compared to PVDF/AOT4-GO/TiO₂ (34.384 L/m² h) (see Table 4). These results further confirmed that embedding triple-tail TC14-GO into the casting solution has improved the dye rejection as well as high permeability in comparison with double-tail AOT4-GO. This was believed related to the extra chain interconnection between GO and PVDF provided by triple-tail TC14 surfactant which resulted higher GO content in the PVDF/TC14-GO/TiO₂ thus improved the hydrophilicity and porosity value. These results lead to the conclusion that the utilisation of a higher surfactant's tail number in the GO synthesis process affected the dye flux and dye rejection efficiency.

Table 4 Dye rejection performance of the fabricated nf membranes measured at a pressure of 2 MPa

Membrane	Dye flux (L/m ² h)	Final concentration (ppm)	Rejection rate (%)
PVDF/AOT4-GO/TiO ₂	34.384	0.760	92.39
PVDF/TC14-GO/TiO ₂	91.106	0.738	92.61

Antifouling Properties of the Fabricated NF Membranes

Assessment of the fabricated NF membranes on long-term performance has been evaluated by their fouling. Filtration activity has caused the dye's organic molecules deposited on the membrane surface then permeate into the membrane which then contributed to the membrane fouling (Nikooe and Saljoughi 2017). Antifouling characteristics of the prepared membranes were then studied through the FRR. Based on Fig. 6, the flux decline curve of PVDF/TC14-GO/TiO₂ decayed rapidly during the first 3 min before being stabilised gradually. Meanwhile, slower flux decline was observed for PVDF/AOT4-GO/TiO₂ which indicated better antifouling properties (Zhu et al. 2017). In general, lower organic adsorption at the membrane surface makes it easier to be cleaned (Zhang et al. 2013). Before the membrane was cleaned, the pure water flux of PVDF/AOT4-GO/TiO₂ and PVDF/TC14-GO/TiO₂ at the same pressure was 38.082 and 100.137 L/m² h, respectively. However, after the membrane was cleaned, the FRR for PVDF/AOT4-GO/TiO₂ was higher (166%) than PVDF/TC14-GO/TiO₂ (119%), indicated an excellent organic molecules adsorption resistance (Wang et al. 2015). This result confirmed that the different GO content in both membranes clearly affects the FRR value. The

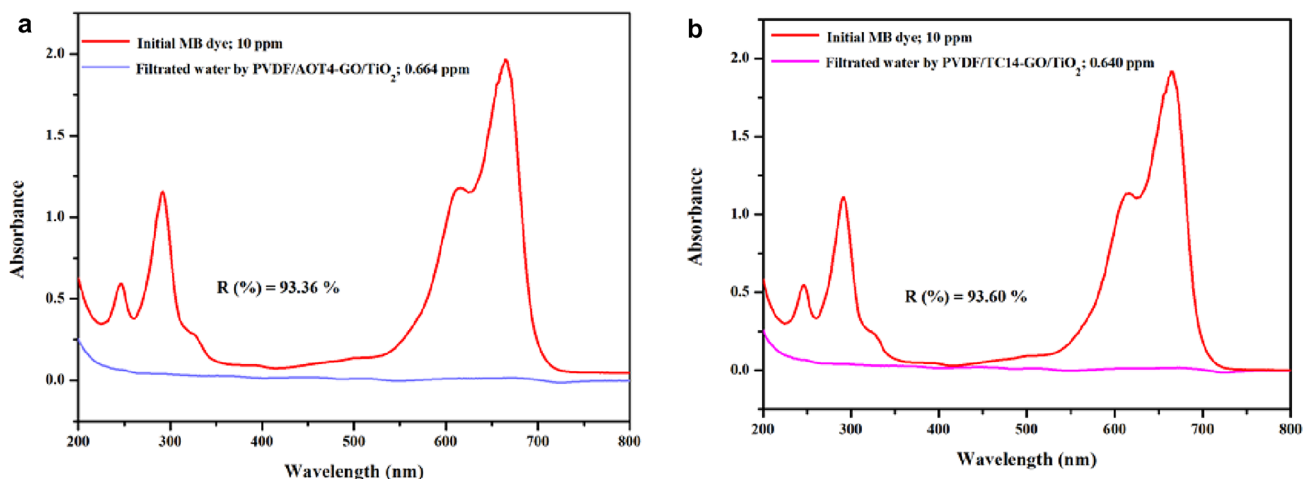
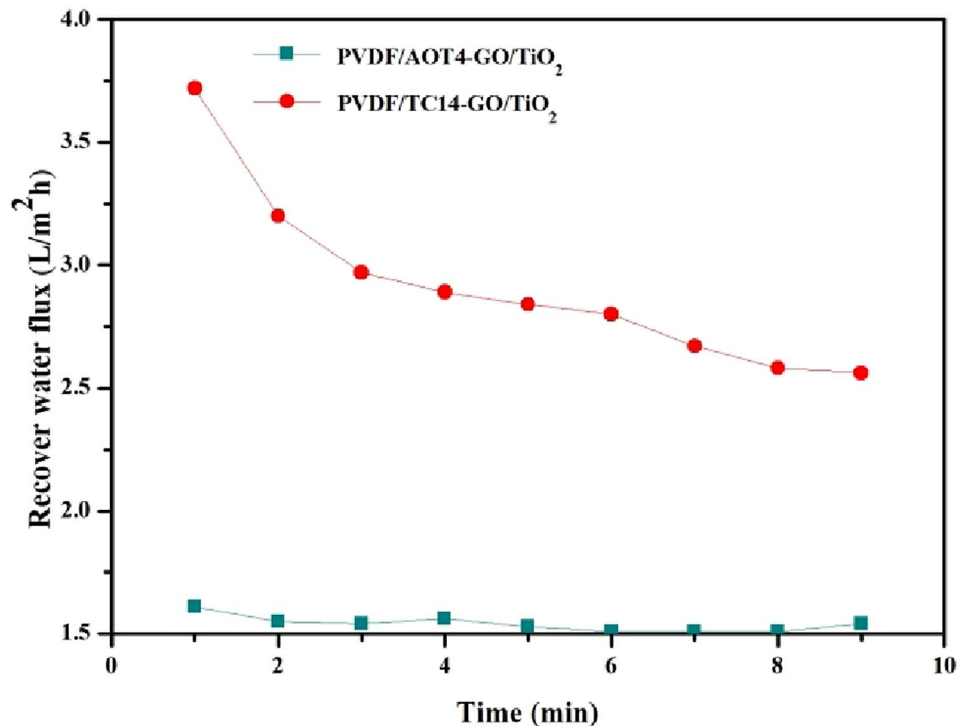


Fig. 5 Dye rejection measurement of the fabricated NF membrane by using UV–Vis spectroscopy; (a) PVDF/AOT4-GO/TiO₂ and (b) PVDF/TC14-GO/TiO₂

Fig. 6 Flux decline curve of the fabricated NF membranes measured at 2 MPa pressure



lower FRR value presented by PVDF/TC14-GO/TiO₂ was believed due to its large pores size which leading to some fouling blocked and adsorbed onto the membrane surface. Therefore, the volume available for passage of the permeate were then reduced (Coutinho et al. 2009).

Conclusions

In this work, PVDF/AOT4-GO/TiO₂ and PVDF/TC14-GO/TiO₂ NF membranes were successfully fabricated via NIPS method utilising customised double-tail AOT4 and triple-tail TC14 surfactants for GO synthesis via electrochemical exfoliation. Based on several measurements, it was found that the utilisation of a higher surfactant's tail number resulted in larger macro-voids structure with higher membrane's porosity and pore size. In addition, higher membrane hydrophilicity was also achieved as the contact angle decreased. PVDF/TC14-GO/TiO₂ presented three times higher water permeability (48.968 L/m² h MPa) and dye flux (91.106 L/m² h). Moreover, its FRR high value (119%) indicated good antifouling performance. The obtained results suggest that the addition of TiO₂ and different type of GO as additives play an important role to enhance the dye rejection and antifouling performance.

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